

Fabrication, Performances and Aging of Flexible Gas Sensor Platforms

Beatriz Medina-Rodriguez^{1*, 2}, Francisco Ramos¹, Giovanni Vescio², Xavier Arrese², Aïda Varea² and Albert Cirera²

1. *Advanced Materials Dept., FAE-Francisco Albero S. A. U., L'Hospitalet de Llobregat 08908, Spain*

2. *Department of Electronics, University de Barcelona, Barcelona 08028, Spain*

Abstract: Flexible electronics are attracting much interest in gas sensor field on on-site monitoring applications due to their wear ability, lightweight and low-cost production. These performances are fully accomplished by silver-based platforms, but silver corrosion represents the main drawback for the integrity of the devices. In this work, self-heating sensor platforms fabricated by screen- and inkjet-printing techniques have been developed. The reliability of both types of sensors has been tested by long-term lifetime characterization and aging tests. These tests proved that the actuation time is interrupted by silver corrosion phenomena in screen-printing devices and by hot spots in inkjet-printing ones. Appropriate solutions regarding isolation and design improvements achieved not only an increase of lifetime and reliability, but also a decrease of power consumption.

Key words: Inkjet printing, screen printing, silver corrosion, flexible gas sensor.

1. Introduction

Global market demands for high quality and low-cost electronic devices. Printing techniques onto flexible polymeric substrates not only can lower the production costs but also offer the possibility to fabricate lightweight and wearable devices, unlike traditional electronic fabrication techniques such as monolithic silicon electronics using lithography and other patterning techniques [1-5].

Printed techniques have a high potential due to the possibility to work under room temperature and ambient pressure allowing a low-cost production [6]. SP (Screen-printing) is one of the main conventional and mature printing techniques, often used for simple industrial tasks (text printing and resist etch) and also complex tasks (printing conductors for flexible electronics and keypads). SP has demonstrated to be a useful technique in high-volume devices production; however, the need of masks makes the process

tiresome for short series or customized products. For this reason, industrial companies search for new forms of printing techniques.

In the case of IP (Inkjet-printing), individual and micrometric drops are deposited onto the substrate on demand. The precise drop deposition opens the possibility of printing very thin conductive paths, minimizing both, device size and material expenses as well as the time and cost saving due to the ease in accomplishing design changes where the mask is not needed. IP is still under development and shows a huge challenge in terms of performance and reproducibility compared to matured techniques such as SP, and also in the current assortment of functional materials available on the market [8].

PET (Polyethylene terephthalate) and PEN (Polyethylene naphthalene) are both highly widespread as substrates in the current flexible electronic industry [9-14]. Nevertheless, PET and PEN have low thermal resistance and become unstable at temperature beyond 80 °C and 140 °C, respectively, and lose their mechanical properties. Up these

Corresponding author: Beatriz Medina-Rodriguez, Ph.D. student, research field: printed electronics. E-mail: b.medina@fae.es.

temperatures some others polymers, such as PI (Polyimide) are required for the post-treatment of the functional material [13, 15]. PI can endure a widest temperature range. Its glass transition temperature is 360 °C what enhances its potential application in different technological fields.

Regarding printed materials; silver is the most widely used conductive material in flexible electronics. Its excellent electrical conductivity and the possibility to be sintered at low temperatures (lower than 300 °C) make it a good prospect for flexible devices. Even so, silver corrodes easily in industrial environments containing sulfide [17] or in outdoor applications due to the humidity [18] and chloride [19] even not near saltwater sources where there are inland chloride species, such as ClNO_2 [20]. Therefore the reliability of the devices is highly compromised.

In this work, a comparison between low-cost flexible sensor platforms fabricated by means of SP and IP techniques has been developed. The performance of the sensor platforms was checked by long-term characterization and aging tests to identify the causes of the device failure. Design improvement to overcome the drawbacks of silver corrosion and power consumption has been achieved, obtaining a sturdy, wearable and reliable gas sensor platform.

2. Experimental Setup

2.1 Techniques and Materials

For the SP-devices a paste based on silver flakes (C2080415D2 from Gwent Group) was used as the conductive material to print the sensing and the heating parts of the gas sensor platform (Fig. 1a). Apical® PI from Sertek was used as the substrate and the SP process has been carried out with a DEK Horizon 03i. After printing, the silver paste was cured at 135 °C during 15 min in a box oven. These SP-devices were fabricated in FAE Company.

The IP-devices were printed with a Xenjet 4000 from Xennia Technology Ltd. The cartridge was a Xaar 126/50, based on piezoresistive technology to

eject the ink. U5603 silver ink with 20 wt% of silver nanoparticles was provided by Sun Chemical. In this case, Kapton® PI from DuPont was used as the substrate. These devices were fabricated in the Electronics Department of the University of Barcelona. The IP-patterns were sintered at 225 °C for 20 min on a box oven. The adhesive PI tape used for the heater isolation was ISOAD 7104 provided by Isovolta.

The devices were calibrated and tested applying voltage pulses and monitoring their temperature by a thermographic camera (NEC Thermoshot F30). Long-term tests were carried out by applying a constant voltage to achieve an initial sensor temperature value of 120 °C. Previous works done in our group showed that these platforms, implemented with carbon nanofibers as sensing material, better respond at 120 °C for NH_3 and NO_2 gas sensing [21]. The tests were interrupted different times to measure the heater resistance at room temperature. The chemical composition of the deposited materials was determined by EDXS (energy dispersive X-ray spectroscopy). The surface morphology of the deposited silver was checked by FE-SEM (field emission scanning electron microscopy). Both EDXS and FE-SEM analysis were carried out on a FE-SEM JEDL J-7100 microscope. Corrosion resistance of the deposits was analyzed by salt-spray chamber and by a

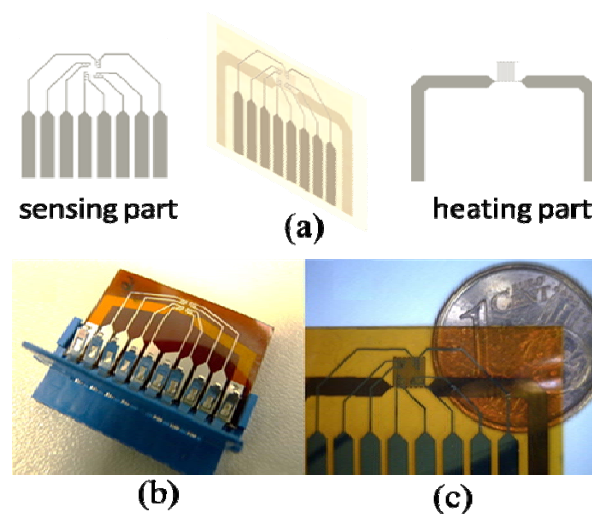


Fig. 1 (a) Scheme of the sensing and heating parts of the printed platforms, (b) SP-printed and (c) IP-printed

devices.

climate chamber. Salt-spray tests were performed with a 50 g/L of NaCl concentration during 72 h while climate chamber tests were performed with 95% humidity using two-hours on/off cycles keeping a temperature constant at 100 °C during 72 h.

2.2 Design and Fabrication

The sensor platform consists of a sensing part and a heater. The sensing part is composed by four interdigitated sensor electrodes and eight connection pads (Fig. 1a). The connection pads were designed in such a way that fit in a clamp-like connector, as it can be seen in Fig. 1b. While sensing part was printed in the topside of the PI tape, the heater was printed on the bottom side, being located just in the area where the printed electrodes are allowing heating up the sensing part. This kind of design (Fig. 1c) is already proved to be suitable for gas sensors [21]. The line width of the interdigitated electrodes and the line strip of the heater were 100 μm and 150 μm , respectively.

3. Experimental Results

Once the devices were fabricated by means of SP and IP, heaters were calibrated. The sensing part temperature is plotted as a function of heater power consumption (Fig. 2). Both platforms showed similar behavior; the sensor temperature linearly increases as power consumption of the heater is higher, achieving around 120 °C for 200 mW. This means that with SP and IP techniques, it is possible to fabricate devices with similar initial electrical characteristics.

To check the endurance of the heaters, a long-term test was carried out. It is known that silver oxidizes quicker as the temperature increases [22], so the heaters were connected to a voltage source to increase the sensor part temperature up to 120 °C. Meanwhile, this temperature was kept constant; the printed devices were maintained in continuous operation until their failure. The heater electrical resistance was measured in different times of the test (square pattern line of Fig. 3a and b). After just few hours of operation,

SP-heaters evidenced a change on the surface color, from silvery to brown; this fact clearly indicates the presence of surface corrosion. A total device failure occurred after 300 h (Fig. 3a) where the electrical resistance of the heater increases asymptotically with time. Higher power consumption is needed for the same temperature, which being detrimental for the heater performance and leading to a malfunction of the devices. It is important to underline the fact that all the area which is heated up is degraded quickly; not only the heaters, but the sensing electrodes too. The EDXS analysis showed that only Ag and C elements were present in the as-deposited tracks (Table 1). After the SP-device failure, new elements as S, Cl and O were found, which indicates a change of the track composition due to a surface corrosion. Furthermore, different studies [23-26] show that the porosity and roughness of metal coating surfaces accelerates the corrosion process. The FE-SEM images of SP-printings showed a no-homogenous, porous and full of holes surface, induced by the flake-like structure (Fig. 3c), which makes easier the penetration of the reactive species, like S, Cl and O, into the deposit structure, causing then the premature failure.

Regarding to IP-devices, the total failure occurred in 140 h (square pattern line Fig. 3b), earlier than SP-devices, but no surface corrosion evidences were found. EDXS analysis showed no significant variation on the deposit composition of IP-devices after the

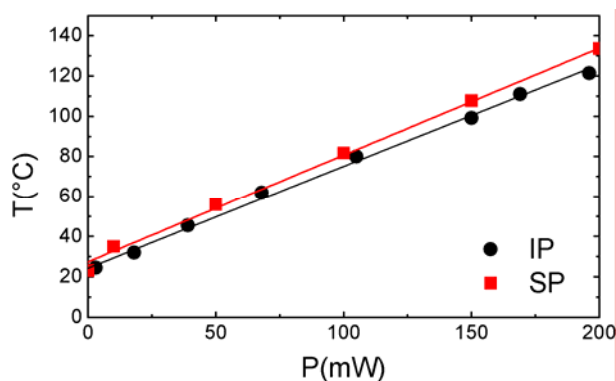


Fig. 2 Calibration plot of SP- and IP-devices. A linear dependence of the temperature of the sensing part is evidenced as a function of heater power consumption.

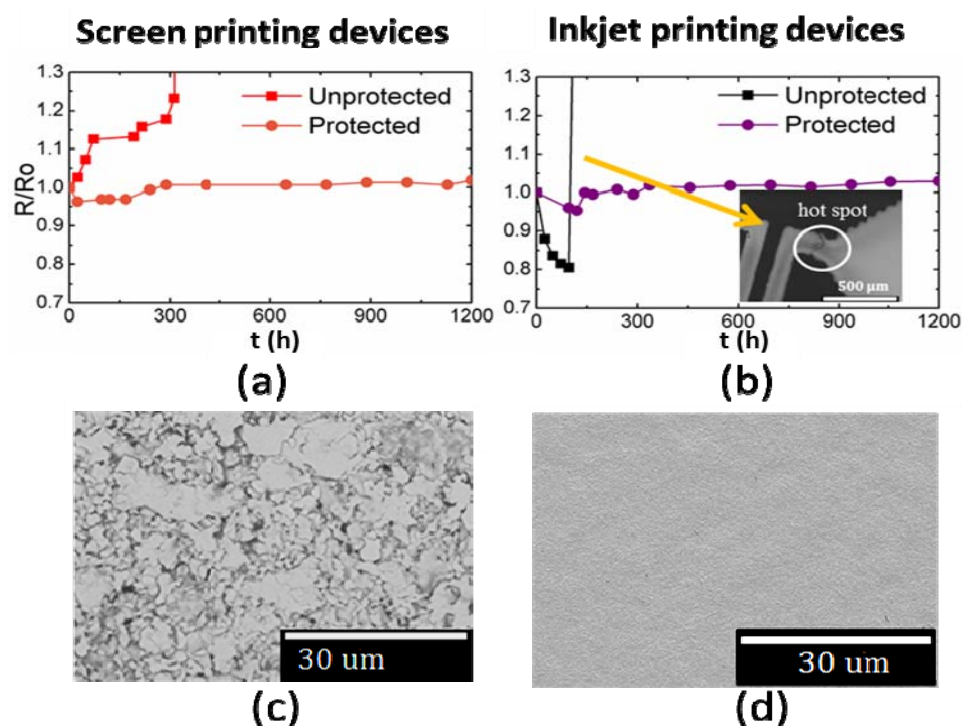


Fig. 3 Electrical performances of (a) SP- and (b) IP- heaters during the continuous operation at 120 °C. FE-SEM images of the silver track printed by (c) screen printing and (d) inkjet printing. Inset: discontinuity on the inkjet-printed heater caused by a hot spot.

Table 1 EDX results for the composition of the printed deposits before and after the long-term test.

Element	SP devices (wt. %)		IP devices (wt. %)	
	Before	After	Before	After
Ag	92	79	98	95
C	8	8	2	3
S	0	6	0	0
Cl	0	3	0	0
O	0	4	0	2

failure (Table 1). FE-SEM images (Fig. 3d) showed a homogeneous surface without the presence of holes or defects. A completely smooth surface is reached by means of the sintering process of the silver nanoparticles. IP-devices showed then an almost inexistent porosity that minimizes the silver exposed to the atmosphere, slowing down the penetration of reactive elements and so the corrosion. Thereby, corrosion is not the cause of these IP-devices failure.

A detailed examination revealed the presence of some discontinuities on the silver tracks after the long-term tests. These discontinuities appeared at vulnerable and weak parts of the design (Fig. 3b) or at

printing defects (bubbles, impurities). Unlike the SP-devices, where the single layer track thickness was around 20 μm , the single printed layer of the IP-tracks was 300 nm thick, what might promote the formation and the fast evolution of cracks and hot spots in a short period of time.

The aging tests showed more obvious the penetration of the reactive species into the silver deposit structure. The SP-heater resistance was increased around 7.6% and 10% after the climate and the salt-spray chambers exposure, respectively. However, for IP-devices the increase of the resistance was quite low; 1.3% and 2.7% for climate and spay-salt chambers, respectively, lower than SP-devices (Table 2).

With the aim to improve the life-time of the designed platforms and to prevent the premature failure of both, SP- and IP-devices, an atmospheric isolation of the silver heaters by a suitable adhesive PI tape was carried out. The sensing part has to be exposed to atmosphere to work as a gas sensor device,

thereby it cannot be isolated. It has to be noticed that after the device protection, devices were laminated to remove all the air that could be trapped between the two layers. By means of the heater protection, long-term test showed an increase of the lifetime of protected SP- and IP-devices more than ten times compared with the un-protected ones (circle pattern line in Fig. 3a and Fig 3b). No degradation after 1,000 h of continuous operation at 120 °C and no consequential deterioration on the device performance were observed. However, the SP-electrodes of the sensing part, which could not be protected from the atmosphere, corroded in few hours due to the porous presence, as it was previously mentioned. Instead, the IP-devices showed no corrosion on the electrodes after 1,000 h of continuous operation. Furthermore, it has been demonstrated that heater protection not only improves SP- but also the IP-devices. The aging tests carried out on the protected devices revealed smaller increase of electrical resistance than for unprotected-devices. An increase around 0.6% and 2% was observed in the case of SP-devices for climatic and salt-spray chambers, respectively. No significant variation in electrical resistance of IP-devices was measured. Then, long-term reliability was achieved by means of the heater protection for both SP- and IP-devices, just the unprotected electrodes made the difference.

At this point, it seems that IP-technique can be pointed as the best route to fabricate such flexible sensing platforms. For this reason, IP heater design was optimized to achieve lower power consumption. As said previously, the very first devices showed a power consumption of almost 200 mW at a temperature of 120 °C (Fig. 2). For new design, the heated area was reduced by narrowing the strips as it is shown in Fig. 4a. Once these changes were carried out, the power consumption was reduced to 125 mW at 120 °C for protected inkjet-printed heaters (Fig. 4b) which implies a reduction of a 38% on power consumption, which value also correspond to the

heating area reduction.

Silicon technology is energetically a little more efficient, around few tens of mW for 200 °C [27, 28], but the fabrication process is extremely expensive and time consuming. An alternative can be the ceramic technology because it is cheaper, but in this case the power consumption increases excessively on the order of hundred times more [29, 30], as well than on glass-based devices [31]. Therefore, the methodology here proposed can be considered like a good alternative to both technologies, reaching a low-consumption and low-cost sensor platform.

Additionally, it has to mention that this novel flexible-platform was implemented with deposited carbon-based materials as the gas sensing material, by means of electrospray technique. The success of this system has been proved in Ref. [21] by measuring different gases such as NH₃ or NO₂.

Table 2 Variation of the electrical resistance for the different devices after the aging test.

	Salt-spray chamber test $\Delta R/R_0$ (%)	Climate chamber test $\Delta R/R_0$ (%)
SP	10.0	7.6
Protected SP	2.0	0.6
IP	2.7	1.3
Protected IP	0.1	0.1

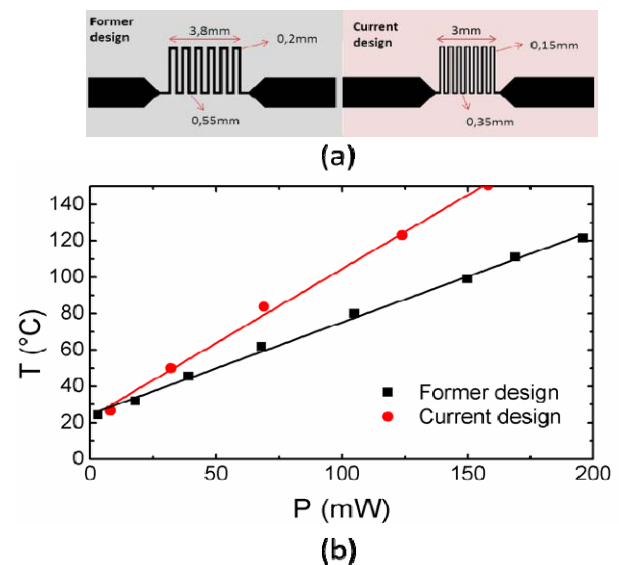


Fig. 4 (a) Scheme and dimensions of the heaters; (b) Sensor temperature as a function of the heater power consumption.

4. Conclusions

Flexible gas sensor platforms fabricated by means of screen- and inkjet-printing were tested by long-term tests maintaining 120 °C during heater operation. Early device failure, caused by chemical degradation, is observed in SP-devices due to the flake-like morphology of the deposits. No noticeable deterioration occurs in IP-conductive tracks of silver nanoparticles. However, the very thin film obtained by inkjet printing promotes a failure by hot spot phenomena. Both kinds of failure are prevented by the heaters isolation from the atmosphere by an adhesive PI tape. The SP- and IP-devices lengthen their life time more than 10 times the unprotected ones. The homogeneity and the smooth surface of IP-devices make them being operative more time than SP-ones. For IP-devices, an improvement of the heater design by reducing the exposed area has shown a decrease of power consumption of 38%, what position the sensor platform as a low-cost and low-powered consumer device. It has been demonstrated that the synergetic combination of polymeric substrates with printed electronics is a good alternative to substitute the monolithic silicon and the ceramic technologies.

Acknowledgments

Albert Cirera acknowledges financial support from ICREA Academia program. Beatriz Medina-Rodriguez acknowledges financial support from Doctorat Industrial program (ACCIÓ-Generalitat de Catalunya).

References

- [1] Zardetto, V., Brown, T. M., Reale, A. and Di Carlo, A. 2011. "Substrates for Flexible Electronics: A Practical Investigation on the Electrical, Film Flexibility, Optical, Temperature, and Solvent Resistance Properties." *Journal of Polymer Science Part B: Polymer Physics* 49: 638-48.
- [2] MacDonald, W. A., Looney, M. K., MacKerron, D., Evesn, R., Adam, R. and Hashimoto, K. et al. 2007. "Latest Advances in Substrates for Flexible Electronics." *Journal of the SID* 15 (12): 1075-83.
- [3] Bao, Z. 2000. "Materials and Fabrication Needs for Low-Cost Organic Transistor Circuits." *Advanced Materials* 12 (3): 227-30.
- [4] Sankir, N. D. 2005. "Flexible Electronics: Materials and Device Fabrication." Ph.D. Thesis, Virginia Polytechnic Institute and State University in Blacksburg.
- [5] Menard, E., Meitl, M. A., Sun, Y., Park, J. U., Shir, D. J. L. and Nam, Y. S. et al. 2007. "Micro-and Nanopatterning Techniques for Organic Electronic and Optoelectronic Systems." *Chemical Reviews* 107 (4): 1117-60.
- [6] Kebs, F. C. 2009. "Fabrication and Processing of Polymer Solar Cells: A Review of Printing and Coating Techniques." *Solar Energy Materials & Solar Cells* 93 (4): 394-412.
- [7] Perelaer, J. and Schubert, U. S. 2010. "Inkjet Printing and Alternative Sintering of Narrow Conductive Tracks on Flexible Substrates for Plastic Electronic Applications, Radio Frequency Identification Fundamentals and Applications, Design Methods and Solutions." In *InTech*, edited by Turcu, C., 324.
- [8] Hudd, A. 2010. "The Chemistry of Inkjet Inks." in: (Ed.), *WorldScientific, New Jersey-London-Singapore*, edited by Magdassi, S.3-18.
- [9] Sun, Y., and Rogers, J. A. 2007. "Inorganic Semiconductors for Flexible Electronics." *Advanced Materials* 19: 1897-916.
- [10] Sazonov, A., Striankhilev, D., Lee, C.-H., and Nathan, A. 2005. "Low-Temperature Materials and Thin Film Transistors for Flexible Electronics." In *Proceedings of the IEEE* 93 (8): 1420-8.
- [11] Hu, A., Guo, J. Y., Alarifi, H., Patane, G., Zhou, Y. and Compagnini, G. et al. 2010. "Low Temperature Sintering of Ag Nanoparticles for Flexible Electronics Packaging." *Applied Physics Letters* 93: 153117.1-7.3.
- [12] Jahn, S. F., Blaudeck, T., Baumann, R. R., Jakob, A., Ecorchard, P. and Rüffer, T. et al. 2010. "Inkjet Printing of Conductive Silver Patterns by Using the First Aqueous Particle-Free MOD Ink without Additional Stabilizing Ligands." *Chemistry of Materials* 22 (10): 3067-71.
- [13] Kim, D., and Moon, J. 2005. "Highly Conductive Ink Jet Printed Films of Nanosilver Particles for Printable Electronics." *Electrochemical and Solid-State Letters* 8 (11): 30-3.
- [14] Magdassi, S., Grouchko, M., Berezin, O. and Kamyshny, A. 2010. "Triggering the Sintering of Silver Nanoparticles at Room Temperature." *ACS Nano* 4 (4): 1943-8.
- [15] Lee, Y. I., and Choa, Y. H. 2012. "Adhesion Enhancement of Ink-Jet Printed Conductive Copper Patterns on a Flexible Substrate." *Journal of Materials Chemistry* 22 (25): 12517-22.
- [16] Scandurra, A., Indelli, G. F., Spartà, N. G., Galliano, F.,

- Ravesi, S. and Pignataro, S. 2010. "Low-Temperature Sintered Conductive Silver Patterns Obtained by Inkjet Printing for Plastic Electronics." *Surface and Interface Analysis* 42 (6-7): 1163-7.
- [17] Minzari, D., Jellesen, M. S., Moller, P. and Ambat, R. 2011. "Morphological Study of Silver Corrosion in Highly Aggressive Sulfur Environment." *Engineering Failure Analysis* 18 (8): 2126-36.
- [18] Lin, H., and Frankel, G. S. 2013. "Accelerated Atmospheric Corrosion Testing of Ag." *Corrosion* 69 (11): 1060-72.
- [19] Liang, D., Allen, H. C., Frankel, G. S., Chen, Z. Y., Kelly, R.G. and Wu, Y. et al. 2010. "Effects of Sodium Chloride Particles, Ozone, UV, and Relative Humidity on Atmospheric Corrosion of Silver." *Journal of Electrochemical Society* 157: 146-56.
- [20] Lemon, C. E. 2012. "Atmospheric Corrosion of Silver Investigated by X-ray Photoelectron Spectroscopy." Ph.D. Thesis, The Ohio State University.
- [21] Claramunt, S., Monereo, O., Boix, M., Leghrib, R., Prades, J. D. and Cornet, A. et al. 2013. "Flexible Gas Sensor Array with an Embedded Heater Based on Metal Decorated Carbon Nanofibres." *Sensors and Actuators B: Chemical* 187: 401-6.
- [22] Sakai, J., Aoki, L., Ohsaka, K. and Ishikawa, Y. 2005. "Sub-micrometer Order Corrosion of Silver by Sulfur Vapor in Air Studied by Means of Quartz Crystal Microbalance." In *International Corrosion Congress*, 19-24.
- [23] Varea, A., Pellicer, E., Pané, S., Nelson, B. J., Suriñach, S. and Baró, M. D. et al. 2012. "Mechanical Properties and Corrosion Behaviour of Nanostructured Cu-rich CuNi Electrodeposited Films." *International Journal of Electrochemical Science* 7: 1288-302.
- [24] Bersirova, O., Kublanovsky, V., Anufriyev, L. and Rubtsevich, I. 2004. "Corrosion Behavior of Electroplated Silver Coatings." *Materials Science* 10 (1): 11-4.
- [25] Bersirova, O. L. and Kublanovskii, V. S. 2012. "Corrosion Properties of Electrodeposited Thin Coatings of Polycrystalline Silver." *Materials Science* 48 (2): 197-202.
- [26] Kaushik, V. K. 1991. "XPS Core Level Spectra and Auger Parameters for Some Silver Compounds." *Journal of Electron Spectroscopy and Related Phenomena* 56 (3): 273-7.
- [27] Cerdà, J., Cirera, A., Vilà, A., Cornet, A. and Morante, J. R. 2001. "Deposition on Micromachined Silicon Substrates of Gas Sensitive Layers Obtained by a Wet Chemical Route: a CO/CH₄ High Performance Sensor." *Thin Solid Films* 391 (2): 265-9.
- [28] Vilaseca, M., Coronas, J., Cirera, A., Cornet, A., Morante, J. R. and Santamaria, J. 2008. "Development and Application of Micromachined Pd/SnO₂ Gas Sensors with Zeolite Coatings." *Sensors and Actuators B: Chemical* 133 (2): 435-41.
- [29] Moldavan, C., Nedelcu, O., Johander, P., Goenaga, I., Gomez, D. and Petkov, P. et al. 2007. "Ceramic Micro Heater Technology for Gas Sensors." *Romanian Journal of Information Science and Technology* 10 (1): 43-52.
- [30] Jiang, B., Maeder, T., Santis-Alvarez, A. J., Poulikakos, D. and Muralt, P. 2014. "A Low-Temperature Co-Fired Ceramic Micro-Reactor System for High-Efficiency On-Site Hydrogen Production." *Journal of Power Sources* 273: 1202-17.
- [31] Santis-Alvarez, A. J., Nabavi, M., Jiang, B., Maeder, T., Muralt, P. and Poulikakos, D. 2012. "A Nanoparticle Bed Micro-Reactor with High Syngas Yield for Moderate Temperature Micro-Scale SOFC Power Plants." *Chemical Engineering Science* 84: 469-78.